

P034

## CRS-Based Minimum-Aperture Time Migration - A Real Data Example

M. Kienast (Geophysical Institute, University of Karlsruhe), M. Spinner (Geophysical Institute, University of Karlsruhe) & J. Mann\* (Geophysical Institute, University of Karlsruhe)

### SUMMARY

The achievable image quality and the reliability of amplitudes in Kirchhoff migration strongly depend on the selection of the migration aperture. Optimal amplitudes are obtained if the migration aperture is restricted to the constructively contributing part of the reflection event which is related to the size of the projected Fresnel zone. The Common-Reflection-Surface (CRS) stack provides kinematic wavefield attributes that allow to address this problem together with a straightforward time migration velocity model building. The approach is applied to a complex onshore data set and compared to conventional Kirchhoff migration. We observe an improved continuity of the reflection events as well as more stable amplitudes in regions with reliably detected CRS attributes. Moreover, the computational costs of the prestack migration are significantly reduced.

## Introduction

The Common-Reflection-Surface (CRS) stack method provides a set of stacking parameters, so-called kinematic wavefield attributes, which can be utilised in subsequent processing steps. [Jäger \(2005\)](#) employed the CRS attributes in pre- and poststack Kirchhoff depth migration to estimate the size and location of the minimum migration aperture with the aim to reduce migration artifacts and to avoid operator aliasing. As depth migration is quite sensitive to velocity model errors and costly in terms of inversion, we transfer the concept to the time domain. The focus of the time domain approach is to reduce migration artefacts and to provide an improved input for subsequent amplitude-versus-offset (AVO) analysis. In this paper, we present the first application of the approach to real data and a comparison to conventional results.

## Basics of CRS stack

The CRS method is based on a second-order approximation of the kinematic reflection response of an arbitrarily curved reflector segment in depth. This approximation can be entirely expressed in terms of kinematic wavefield attributes defined at the acquisition surface rather than in the subsurface: in 2D, these are the emergence angle  $\alpha$  of the central ray, and the radii  $R_{\text{NIP}}$  and  $R_N$  of wavefront curvature of two hypothetical waves, the so-called NIP and normal wave, respectively. The commonly used hyperbolic approximation can, e. g., be found in [Schleicher et al. \(1993\)](#). Similar to a conventional stacking velocity analysis, the optimum wavefield attributes for each location  $(x_0, t_0)$  are determined automatically by means of coherence analysis. The final results are entire sections of the wavefield attributes  $\alpha$ ,  $R_{\text{NIP}}$ , and  $R_N$ , as well as a coherence section.

## Determination of stationary points

In Kirchhoff migration, the main contribution to the diffraction stack stems from the region where the reflection event is tangent to the migration operator, the vicinity of the so-called stationary point  $x_0$ . As the CRS operator is already tangent to a reflection event in the data, this tangency condition can be directly evaluated by a comparison of the CRS operator slope and the migration operator slope. The searched-for slope  $\beta$  of the ZO reflection event is related to the emergence angle  $\alpha$  of the ZO ray via the near-surface velocity  $v_0$ :  $\tan \beta = 2 \sin \alpha / v_0$ . For time migration with straight rays as considered here, the migration operator as well as its derivatives are given by analytic expressions. In practice, the modulus of the difference between these two slopes is calculated and the location of the minimum is chosen as stationary point. The associated coherence values help to decide whether the stationary point is reliable by applying a user-given threshold.

The concept of the *Common-Reflection-Point (CRP) trajectory* allows to extrapolate the stationary point to finite offset. It is entirely defined in terms of the kinematic wavefield attributes, see [Höcht et al. \(1999\)](#). The approximation provides a superior reference for the centre of the migration aperture compared to the conventional approach which ignores the deviation between Common-Midpoint (CMP) and CRP gathers.

## Estimation of minimum aperture

The final information relevant for minimum migration apertures which can be gained from the attributes is the size of the projected ZO Fresnel zone  $W_F$  (see, e. g., [Mann, 2002](#)). In general, the Fresnel zone size is expected to widen with offset. Unfortunately, this effect is hard to quantify as the velocity model together with the dip and curvature of the reflector has to be considered. However, forward-calculated examples suggest that the widening effect is small for reflectors with moderate dip and curvature. For practical application, the ZO Fresnel zone size as determined from the CRS attributes is always extended by a certain percentage (usually 10 to 20 % depending on the attribute quality) as it is crucial not to underestimate the Fresnel zone for true-amplitude processing. Thus, the small widening effect is already covered and may be neglected. For the data example below, the Fresnel zone was set constant for all offsets, an approximation which appears to be reasonably accurate to obtain reliable amplitudes in this case.

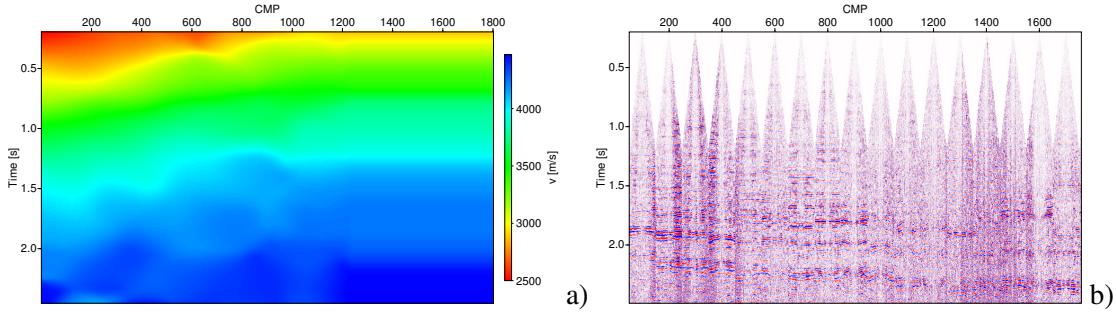


Figure 1: a) Smoothed time migration velocity model determined from the CRS wavefield attributes. b) Several common-image gathers extracted from the conventional time migration prestack data. The maximum offset is 3 km.

### Real data example

To demonstrate the potential of true-amplitude CRS-based Kirchhoff time migration the approach was applied to a complex onshore data set. To gain the kinematic wavefield attributes the highly automated CRS stack method was applied to the real data set.

For the determination of the velocity model, attributes were automatically picked at 2870 data points with high coherence. Reliable picks could only be determined from CMP nos. 1 to 1225. Beyond this location the velocity model was constantly extrapolated in lateral direction. The interpolated velocity model is displayed in Figure 1 together with some common-image gathers extracted from the conventional prestack migration result. An offset-dependent moveout can be clearly observed for the right hand part of the model where, due to the lack of reliable picks, a constant extrapolation has been used.

With the attribute-based time migration velocity model, true-amplitude Kirchhoff poststack time migration was performed twice: on the one hand in a conventional way with a user-defined aperture, on the other hand with the limited aperture given by the projected Fresnel zone. The poststack time migration was processed using the CRS stack section (not shown). The migration target zone consists of a grid with 25 m spatial and 4 ms temporal intervals. The high temporal resolution was chosen to allow a clear separation of closely adjacent reflection events. For the data at hand, the conventional user-given aperture had to be chosen such that the steeply dipping reflector elements located between CMP nos. 500 and 750 and between 1000 and 1100 could be properly imaged. For both approaches a taper was considered in order to suppress artifacts due to border effects.

For all locations where a stationary point has been detected, Figure 2a) shows the projected Fresnel zone. As expected, its size increases with increasing traveltimes and increasing curvature of the reflection events. The large projected Fresnel zones observed, e.g., at CDP 800 and 1.8 s are caused by (fragments of) diffraction events with their typical property  $R_N \approx R_{NIP}$ . There, the theoretical size of the projected Fresnel zone tends to infinity.

In Figure 2b) the horizontal distance between operator apex and stationary point is depicted. It is clearly visible that for flat events the distance tends to zero while on steep events the values of the distance between operator apex and stationary point reach up to 800 m. This demonstrates why a large conventional user-defined aperture is required to capture such events.

To obtain a fully covered image without gaps, the user-defined aperture was utilised at all other locations. This result is shown in Figure 2d). For comparison, Figure 2c) displays the result of the conventional poststack time migration.

In the upper part of the two migrated images only minor differences can be seen, even for the events with significant dip. The good performance of the conventional approach in this area can be explained as follows: for the events with small dips, a comparatively small user-given

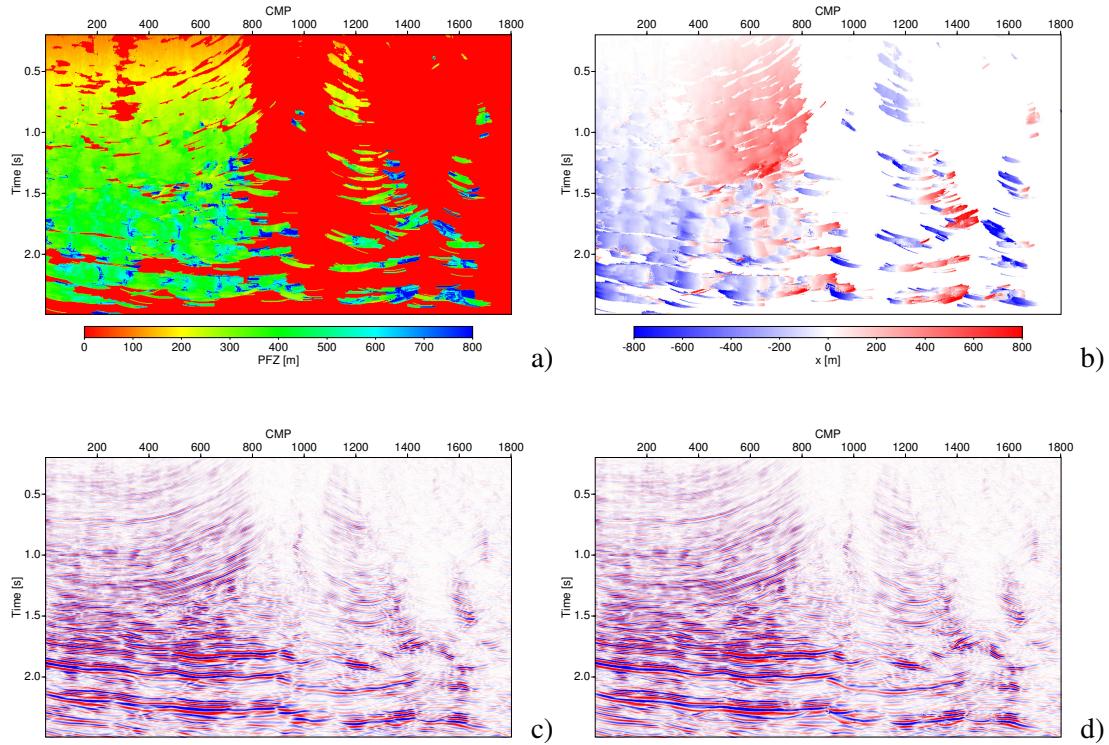


Figure 2: a) Size of the projected first ZO Fresnel zone estimated from the CRS attributes. Only locations with identified stationary points have been considered. b) Horizontal distance between operator apex and stationary point estimated from the CRS attributes. The second row displays the result of the Kirchhoff poststack time migration with c) conventional user-defined aperture and d) with minimum aperture.

aperture can be used without loss of events. The steeper events show a slightly concave structure that leads to a slight decrease in the Fresnel zone size. Therefore, the projected Fresnel zone is still well covered by the user-given aperture although it is displaced with respect to the operator apex.

A closer investigation of the three horizontal reflection events below 1.8 s reveals different effects in the limited-aperture migration result: on the one hand, an improved continuity of these reflection events, for instance at the reflection event between CMP nos. 200 to 400 at 2.15 s, but on the other hand unphysical fluctuations due to unreasonably strong variations of the attributes occurring around CMP no. 900 at 2.3 s. The imaging problem at this area is also complicated by conflicting dip situations which have not been considered for these data. The fluctuations occurring due to varying attributes are usually prevented by a previous event-consistent smoothing of the attributes. However, due to the poor signal-to-noise ratio and low coherence of the data set a reliable smoothing was not possible in this case.

Figure 3a) shows the conventional prestack migration result after muting and stacking over all offsets, whereas in Figure 3b) the corresponding result of the prestack migration with minimum aperture is depicted. As in the poststack case, the user-defined aperture was used at all locations where no stationary point was found. The differences between the two prestack results are comparable to those of the poststack results. The application of the introduced migration technique improved the computational efficiency significantly: compared to conventional migration, the reduction of the required summations led to half of the computational time in the prestack case. The effect on the amplitudes was analysed by extracting an AVO curves from the strong reflector in the common-image gather at CMP 560 in both, conventional and limited-aperture prestack

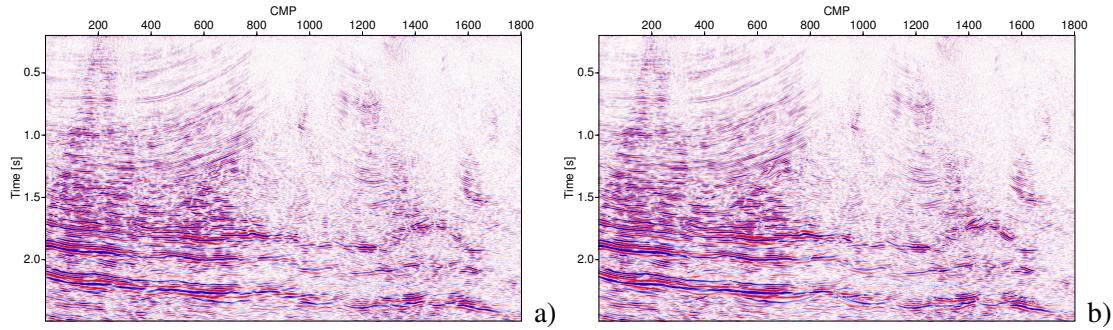


Figure 3: Result of the Kirchhoff prestack time migration with a) conventional user-defined aperture and b) with minimum aperture.

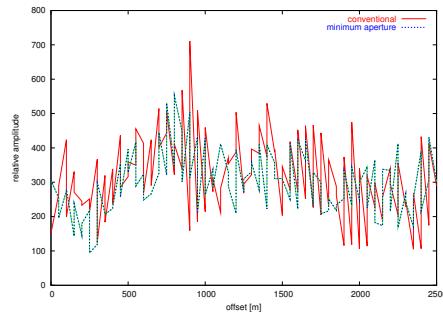


Figure 4: AVO of a strong reflector event at 1.8 s extracted in the common-image gather for CMP no. 560 after true-amplitude prestack time migration with minimum aperture (dashed line) and conventional aperture (solid line).

migration results (Figure 4). A reduction of the noise-related fluctuations can be observed in the limited-aperture AVO plot as just the relevant part of the data was summed up. Hence, AVO analysis benefits from migration with limited aperture.

### Conclusions

Jäger (2005) successfully applied CRS wavefield attributes for minimum-aperture Kirchhoff depth migration. We demonstrated that this concept can be transferred back to the time domain. Here, not only the sensitivity to velocity model errors is reduced, but also the migration velocity model building can be performed in a highly automated and simple way. The entirely analytic migration operators and their corresponding derivatives allow an efficient implementation, especially concerning the determination of stationary points. In this way, we obtain more reliable amplitudes for AVO/AVA analyses compared to conventional approaches.

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### References

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